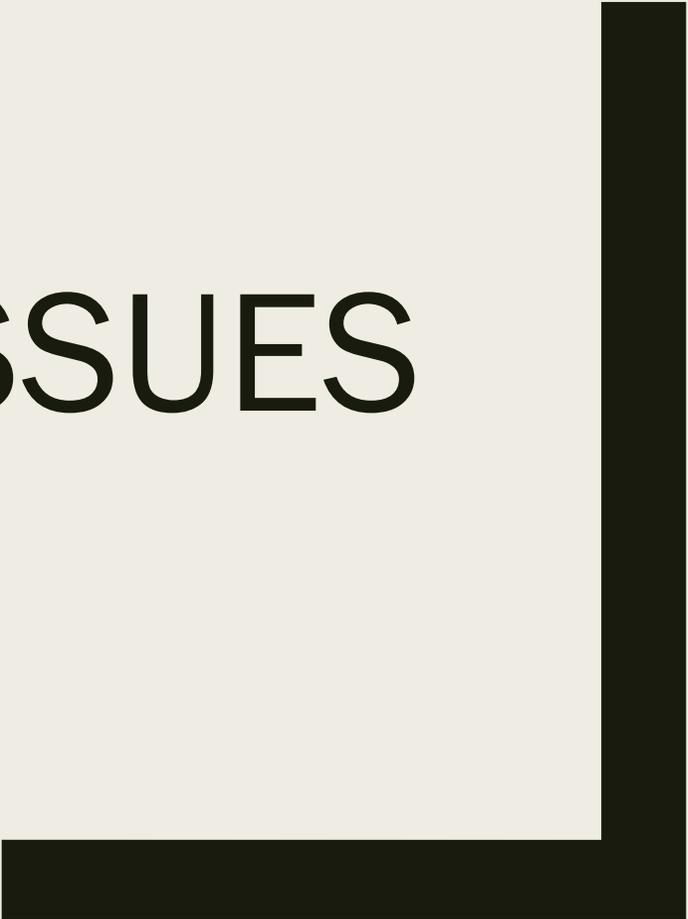




BINDER SPECIFICATION ISSUES

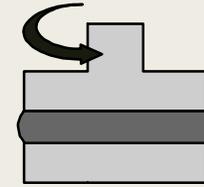
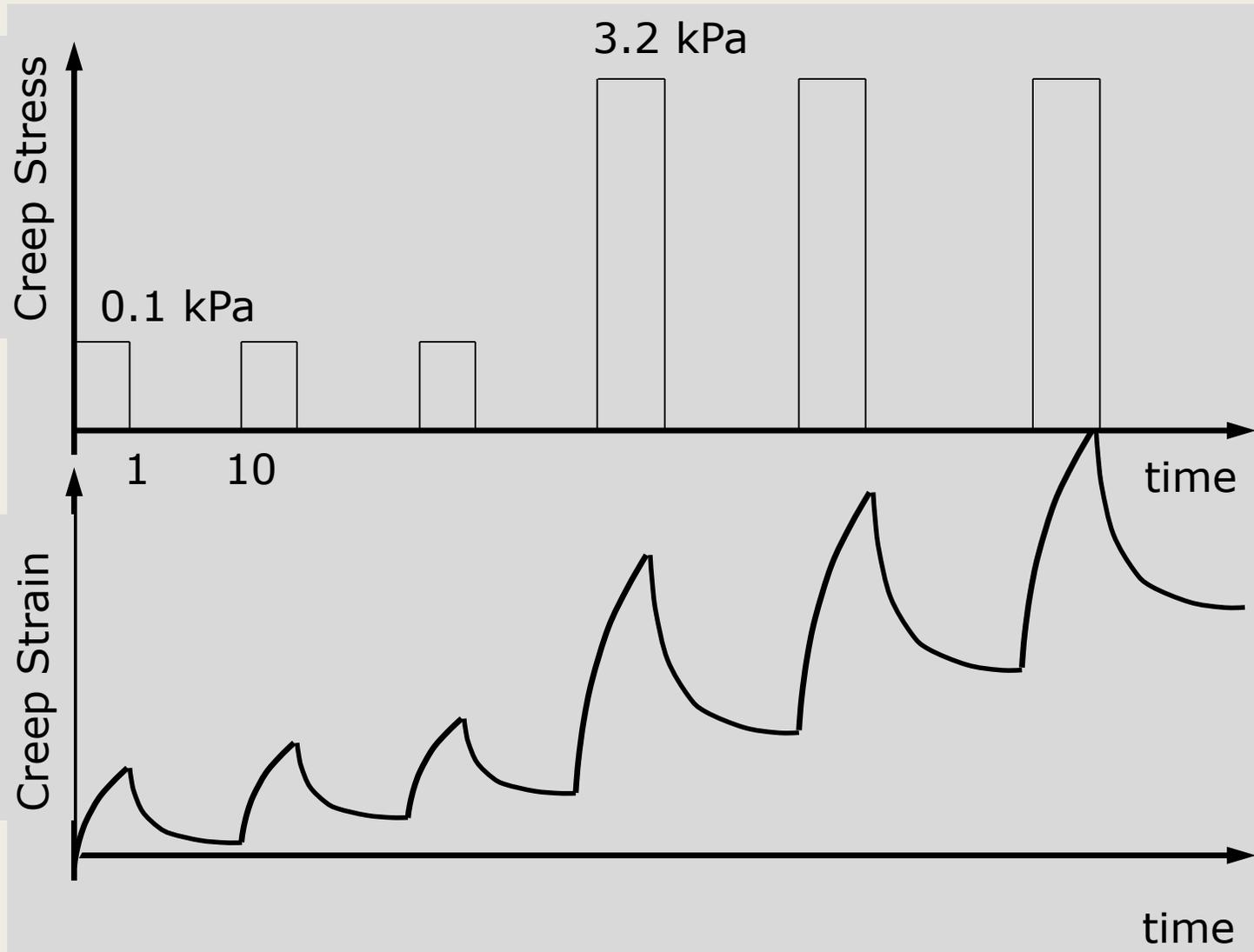
Raj Dongré, Ph.D
Dongre Laboratory Services, Inc.



Outline

- Issues in Asphalt Binder Specifications
 - *MSCR*
 - *REOB*
 - Binder Aging
 - Binder Fatigue
- Impact on Binder Formulation and Grading
 - *Polymer Modification*
 - *Crumb Rubber Modification*
- My Take on Binder Specifications
 - *Wrap Up*

Multi Stress Creep and Recovery MSCR



Test using the DSR applying a 1 sec creep stress followed by 9 sec recovery.

MSCR Test

AASHTO T 350-14 and M 332-14

- Two key values for the MSCR test
- These will determine the binder grade and whether it can be called a PMA binder.

– *Jnr*

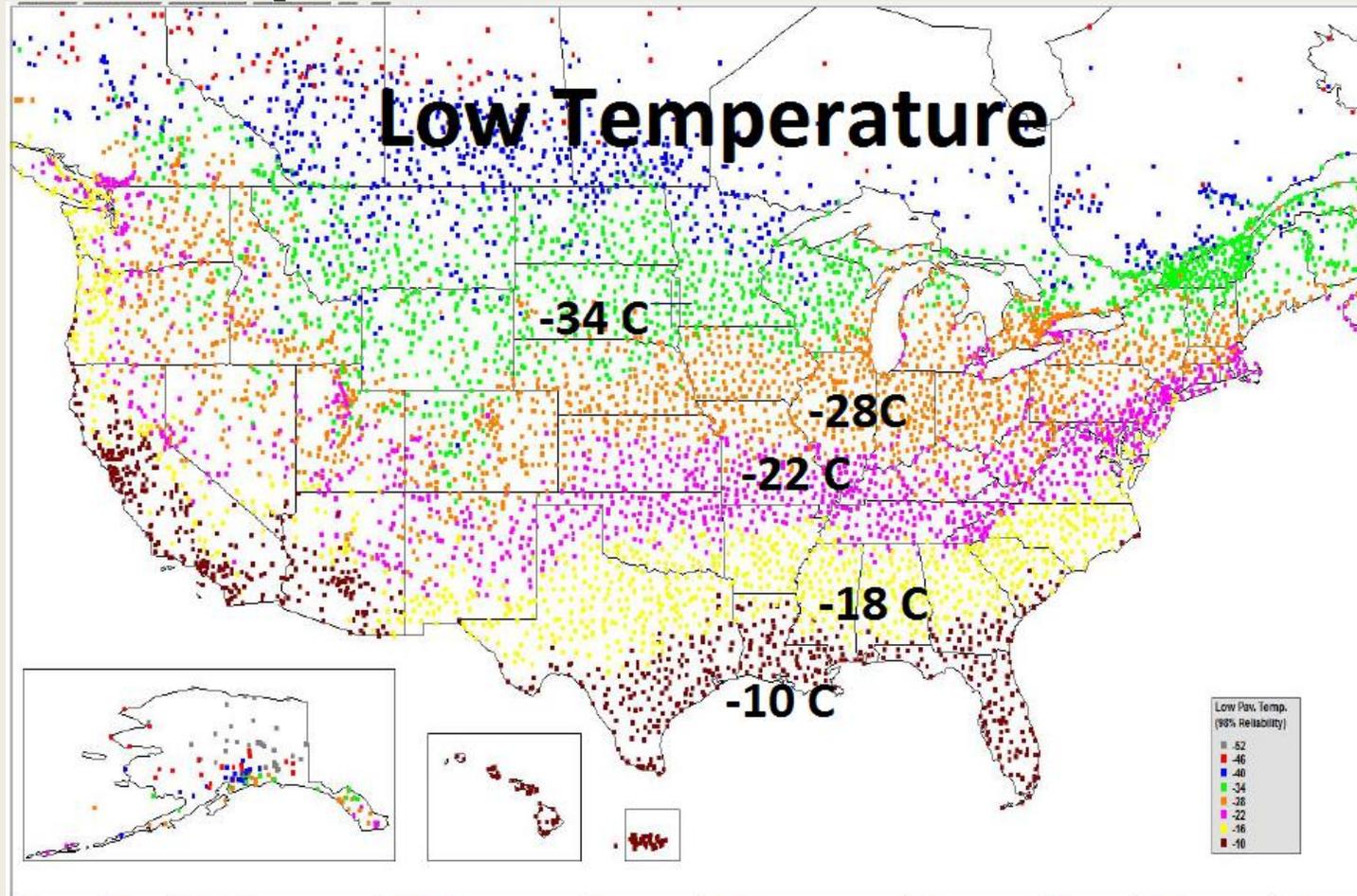
– *% Recovery*

So how do you grade a binder?

Effect of J_{nr} on Lab and Field Rutting

- Reducing J_{nr} by half typically reduced rutting by half.
- This effect is seen on ALF sections and Hamburg Rut Testing
- This is also seen on the Mississippi I 55 sections.

Like PG System, Grade Based on LTPP Climate Temperature



Grade Bumping - NO

- Right now it now it looks like the PG System
- The **BIG** change is that everything is based on the **LOCAL** high temperature environment.
- If environment is 64C
 - *the standard grade, like the PG system is PG 64-22.*
- Other grades, PG 70, and PG 76 will be tested at 64C as PG 64(something), based on the **Jnr**.
- Binder name becomes **state/region dependent**.

MSCR and Low Temperature

- The low temperature tests and nomenclature will not change with MSCR.
- It still uses the BBR results.
- The mid temperature criteria, the 8 mm DSR test, will have 6000 kPa as a cutoff for the stiffer grades, since for DeIDOT the test temp will be 25C.

M - 332 Grades at 64C

- Jnr = 2.0 - 4.5 = PG 64S-22 “Standard” = PG 64-22
- Jnr = 1.0 - 2.0 = PG 64H-22 “Heavy” = PG 70-22
- Jnr = 0.5 - 1.0 = PG 64V-22 “Very Heavy” = PG 76-22
- Jnr = 0.25 - 0.5 = PG 64E-22 “Extreme” = PG 76-22
- Note M - 332 uses “High” & “Heavy” interchangeably
- Standard “S” = traffic < 10 million ESALs, > 70 km/h
- Heavy “H” = traffic 10-30 million ESALs, 20-70 km/h
- Very Heavy “V” = traffic > 30 million ESALs, < 20km/h
- Extreme “E” > 30 million ESALs, < 20km/h, toll plazas

M-320 vs M-332 Grades

- PG 58-28 = PG 58S-28, Jnr 2.0 - 4.5 58C
- PG 64-22 = PG 64S-22, Jnr 2.0 - 4.5 64C
- PG 64-28 = PG 64S-28, Jnr 2.0 - 4.5 64C
- PG 70-22 = PG 64H-22, Jnr 1.0 - 2.0 64C
- No Grade = PG 64V-22, Jnr 0.5 - 1.0 64C
- PG 76-22 = PG 64E-22, Jnr < 0.5 64C and meet polymer elasticity curve.

State DOT Survey - Summary

- Repeatability and Reproducibility
- Jnr Diff. – Not passing for stiff binders
- Nomenclature
 - *S, H, V, E for example PG 64-22V*
- Polymer Dosage
 - *Polymer Curve*
- Quick QC Test during construction
 - *No RTFO*
 - *Able to provide info similar to MSCR RTFO-aged*

Nomenclature in AASHTO M332-14

- Problem:
 - *Correct grades are not being delivered due to the new names*
 - *Truck drivers are confused!!*
- My suggestion:
 - *Change names as follows:*
 - *PG 64-22S → SG 64-22*
 - *PG 64-22H → HG 64-22*
 - *PG 64-22V → VG 64-22*
 - *PG 64-22E → Too Expensive!!*

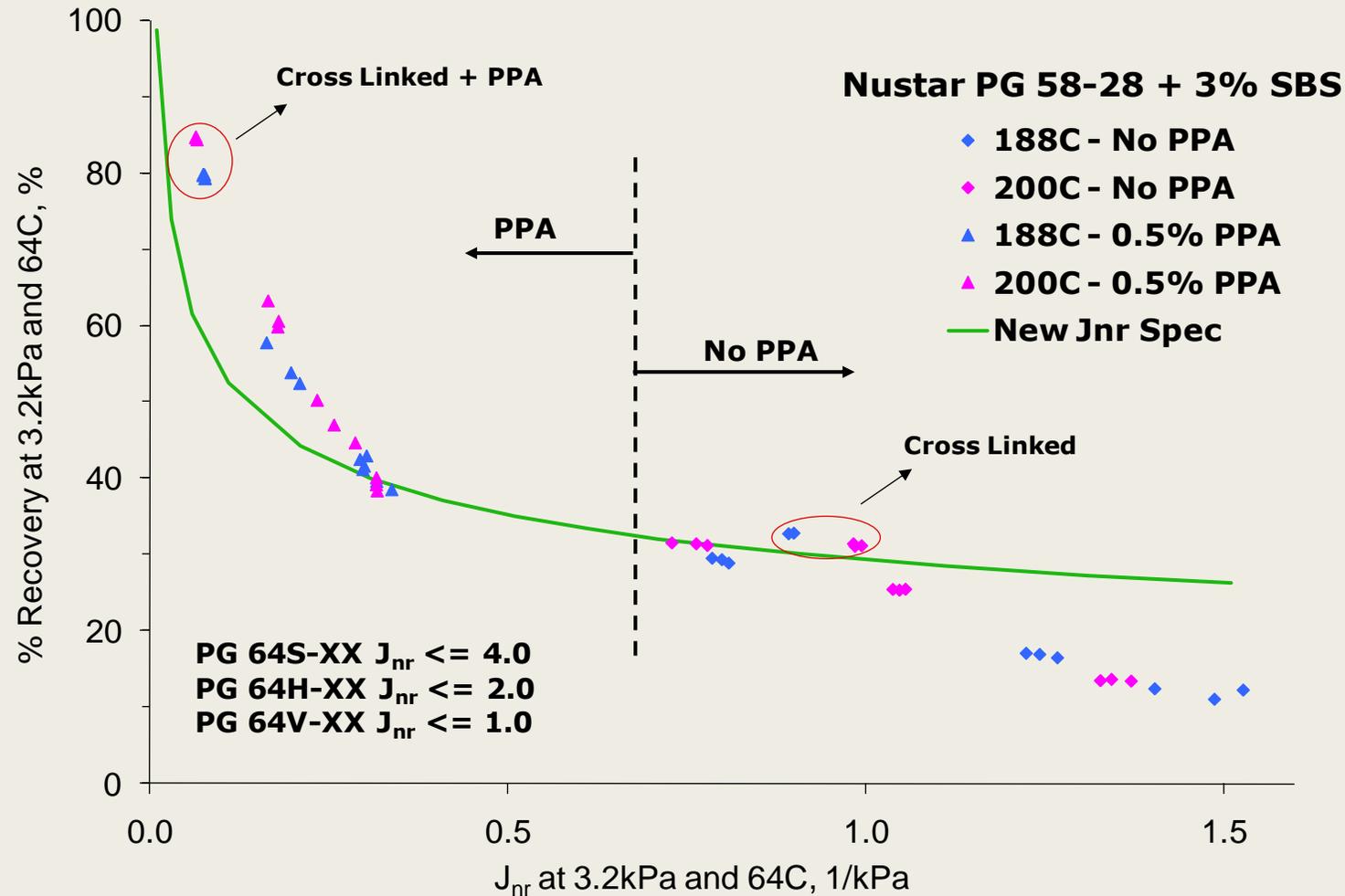
Binder Formulation Challenges

Polymer Modification

- VH and E grades require satisfying the MSCR %Recovery Curve
- MSCR % Recovery Curve Requires that J_{nr} value has an associated % recovery value
 - $\%R = 29.37 * (J_{nr})^{0.263}$ at 3.2 kPa loading
- % Recovery is affected by
 - *Cross-link efficiency*
 - Let downs from concentrates require less polymer to meet % Recovery
 - In earlier PG specification of $G^*/\sin \delta$, phase angle δ was not as sensitive
 - *PPA*
 - *Base Binder Source*

SBS/PPA Asphalt Modification

Polymer Constant



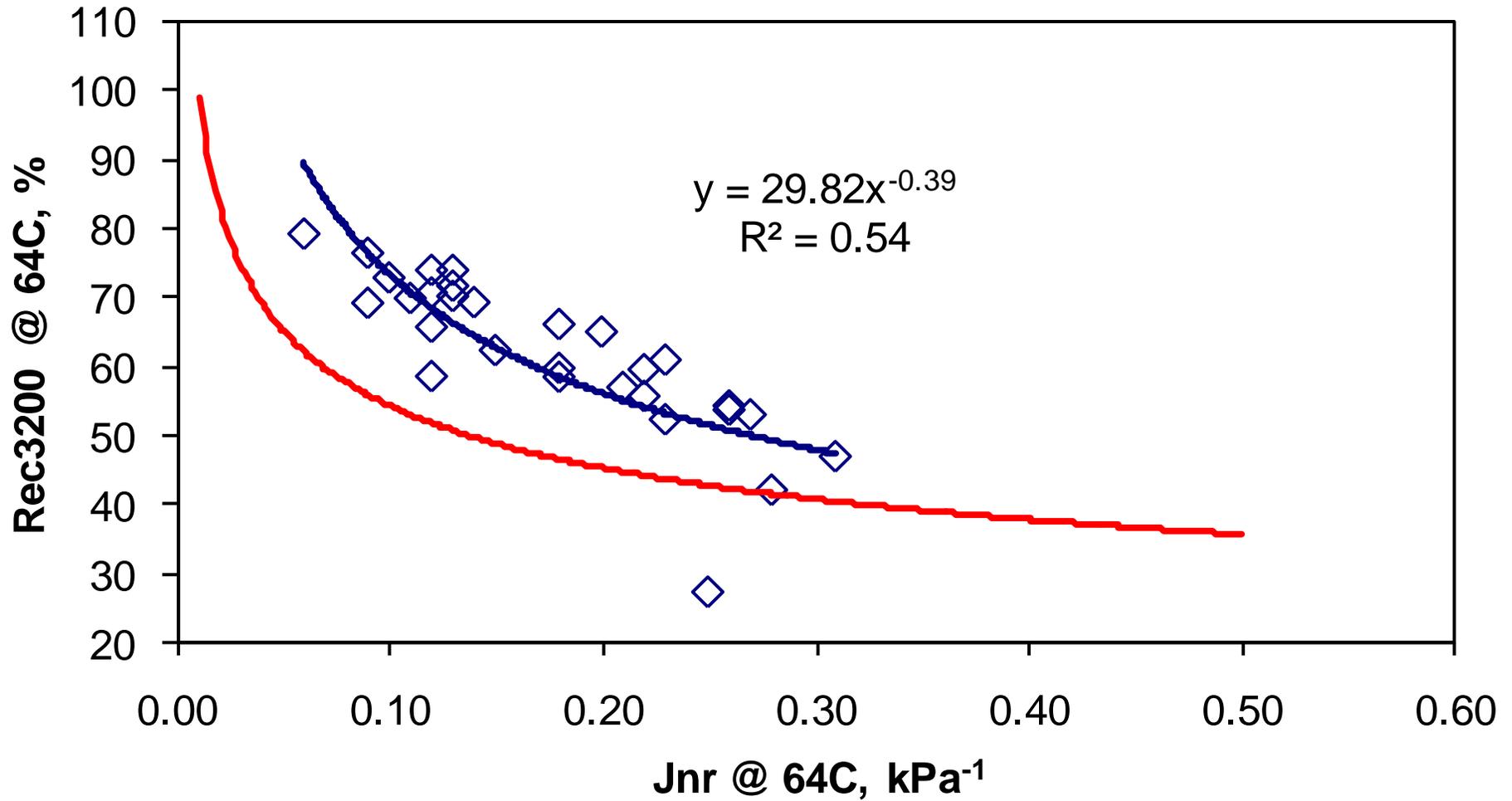
MSCR shows PPA + Polymer is better than either alone.

Binder Formulation Challenges

Crumb Rubber Modification

- Crumb Rubber Modified grades require satisfying the MSCR %Recovery Curve and m-value
 - *FL, GA, LA, NY*
- MSCR % Recovery Curve Requires that J_{nr} value has an associated % recovery value
 - $\%R = 29.37 * (J_{nr})^{0.263}$ at 3.2 kPa loading
- % Recovery and m-value are affected by
 - *Polymer + Crumb Rubber Hybrid*
 - Made by adding crumb rubber to polymer modified binders
 - Use of ECR – crumb rubber pre coated by elastomers
 - *Crumb Rubber Type – Truck Tire Rubber is better*
 - *Base Binder Source*

PG 76-22 Binders: MSCR3200



WHAT IS engineered crumb rubber (ECR)?

- ASTM minus #30 crumb rubber (Truck Tire)
- Rubber Coated with Polymer to meet specific performance criteria:
 - *MSCR – Jnr and % Recovery, BBR - m-value, DSR - Phase Angle*
 - *PG adjustment: upper and lower temperatures*
 - *Penetration, SP, ER, etc.*
 - *Mix Fatigue and Rutting Performance similar to PMB (SBS modified)*

ECR Types

- Standard ECR
 - *30 mesh, 40 mesh with Elastomer coating*
 - *Typical ECR content in CRMB - 10% or less*
- ECR-WMA
 - *Standard ECR with WMA additive coating*
- ECR-MD (moisture damage)
 - *Standard ECR with Anti-strip coating*

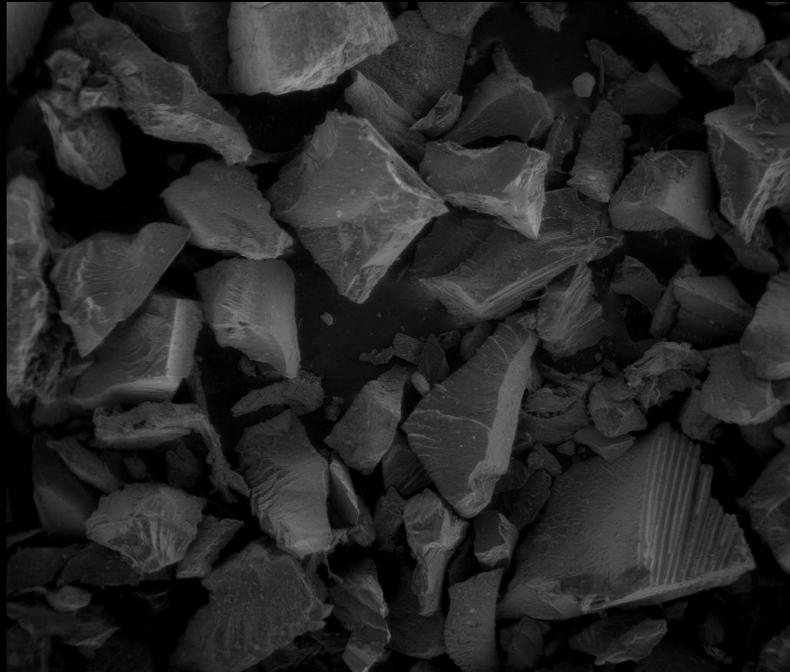
ECR Types.....

- ECR-PPA
 - *Standard ECR with PPA coating*
- ECR-HM (High Modulus Mix)
 - *ECR with higher elastomer coating*
 - *DRY MIX method – used with standard PMA*

WHAT IS ENGINEERED CRUMB RUBBER (ECR)?

- Polymer Coated Crumb Rubber with a Patented Coating Process - -
#30 mesh CRM (0.2 to 0.4 mm)

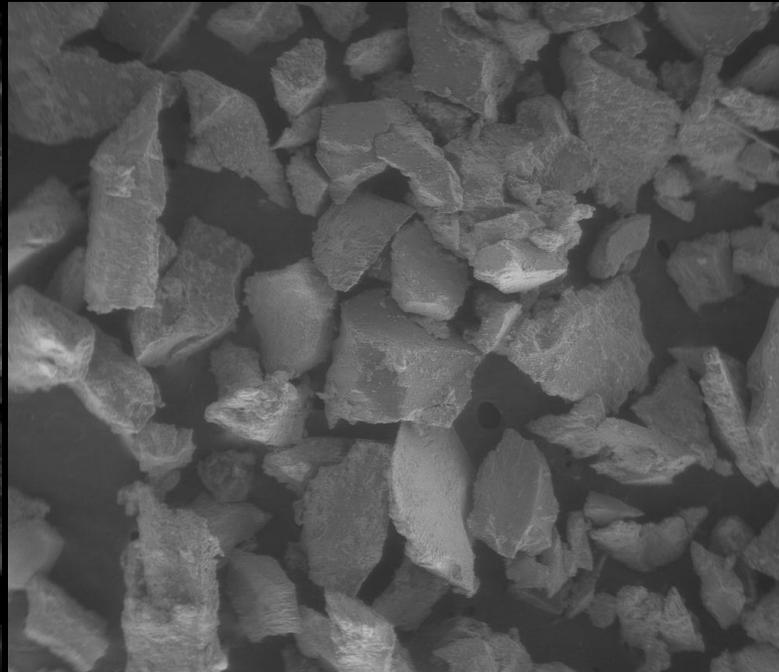
Normal Crumb Rubber



HV	det	WD	mag	HFV
5.00 kV	LFD	7.9 mm	50 x	2.98 mm

1 mm
label

Engineered Crumb Rubber



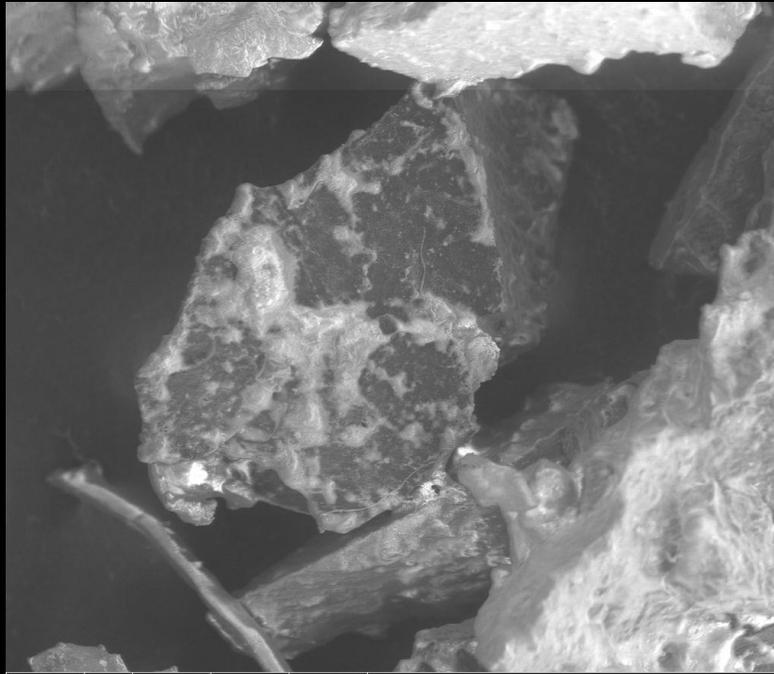
HV	det	WD	mag	HFV
5.00 kV	LFD	8.5 mm	50 x	2.98 mm

1 mm
label

WHAT IS ENGINEERED CRUMB RUBBER (ECR)?

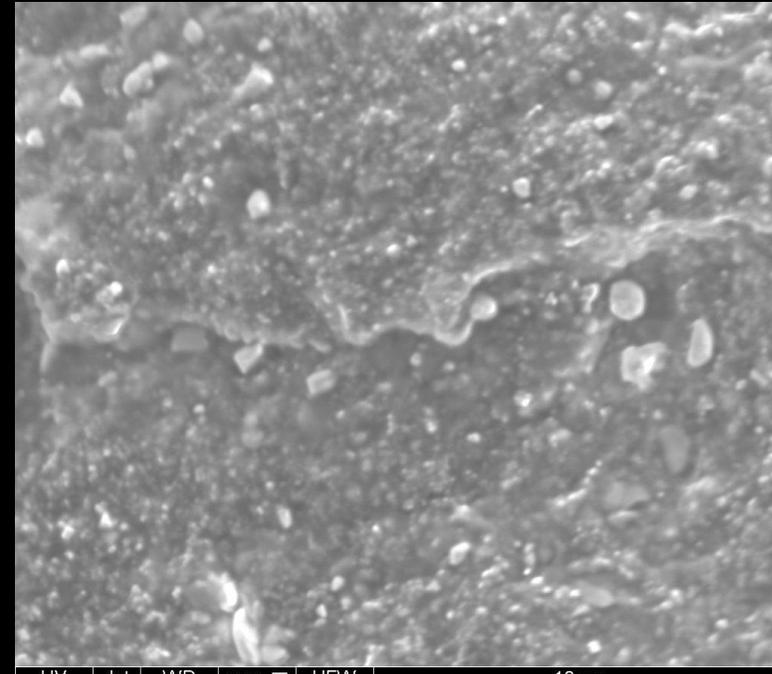
- Polymer Coated Crumb Rubber with a Patented Coating Process - - #30 mesh CRM (0.2 to 0.4 mm)

ECR at 180x mag.



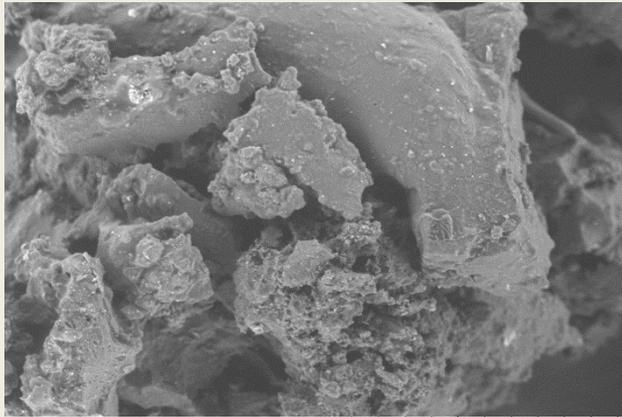
HV	det	WD	mag	HFW	400 μm
5.00 kV	LFD	5.3 mm	180 x	829 μm	label

ECR at 5000x mag.

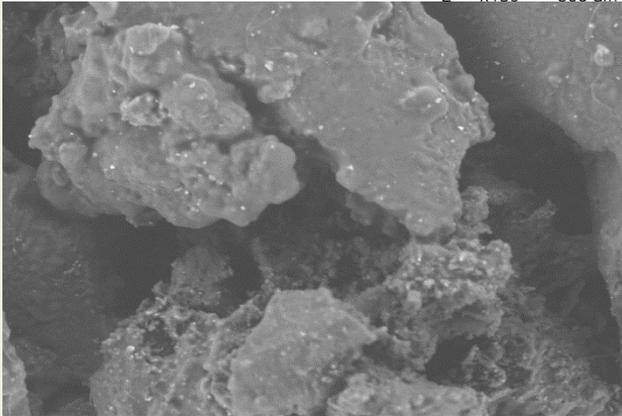


HV	det	WD	mag	HFW	10 μm
5.00 kV	LFD	4.7 mm	5 000 x	29.8 μm	label

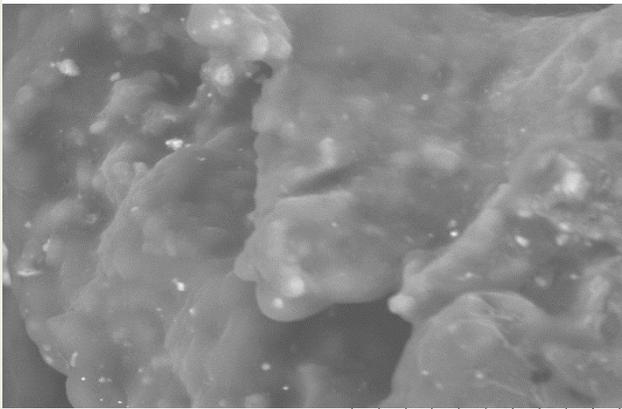
-30 mesh



L x180 500 um

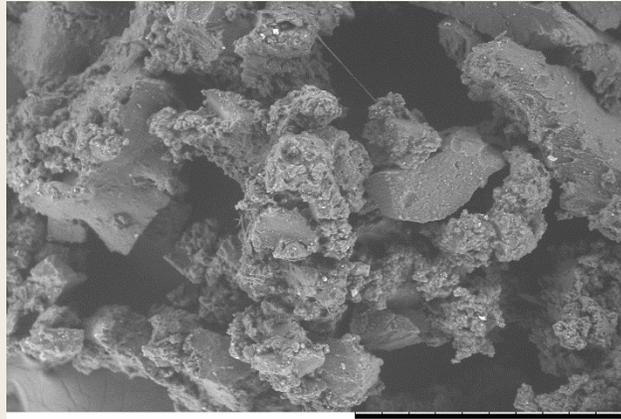


L x500 200 um

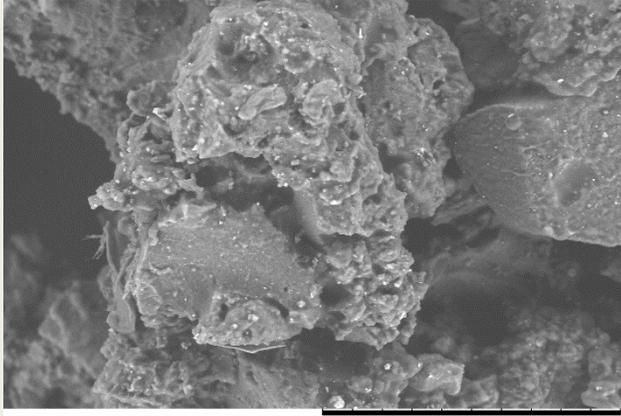


L x3.0k 30 um

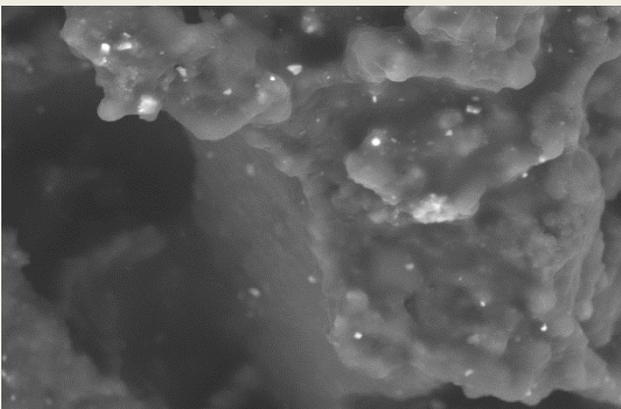
-40 mesh



L x180 500 um

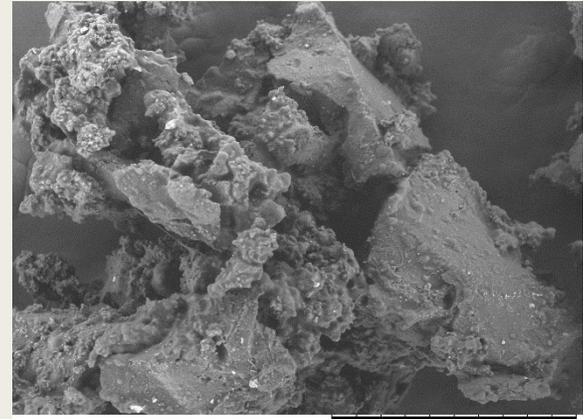


L x500 200 um

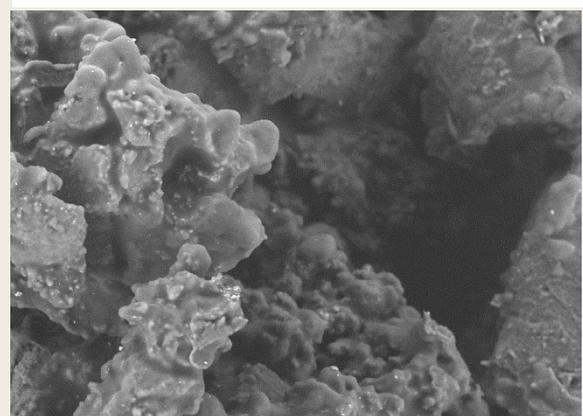


L x3.0k 30 um

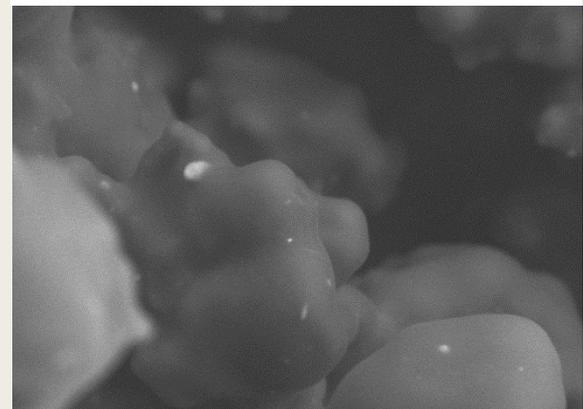
-30 mesh - Dual Polymer



L x180 500 um



L x500 200 um

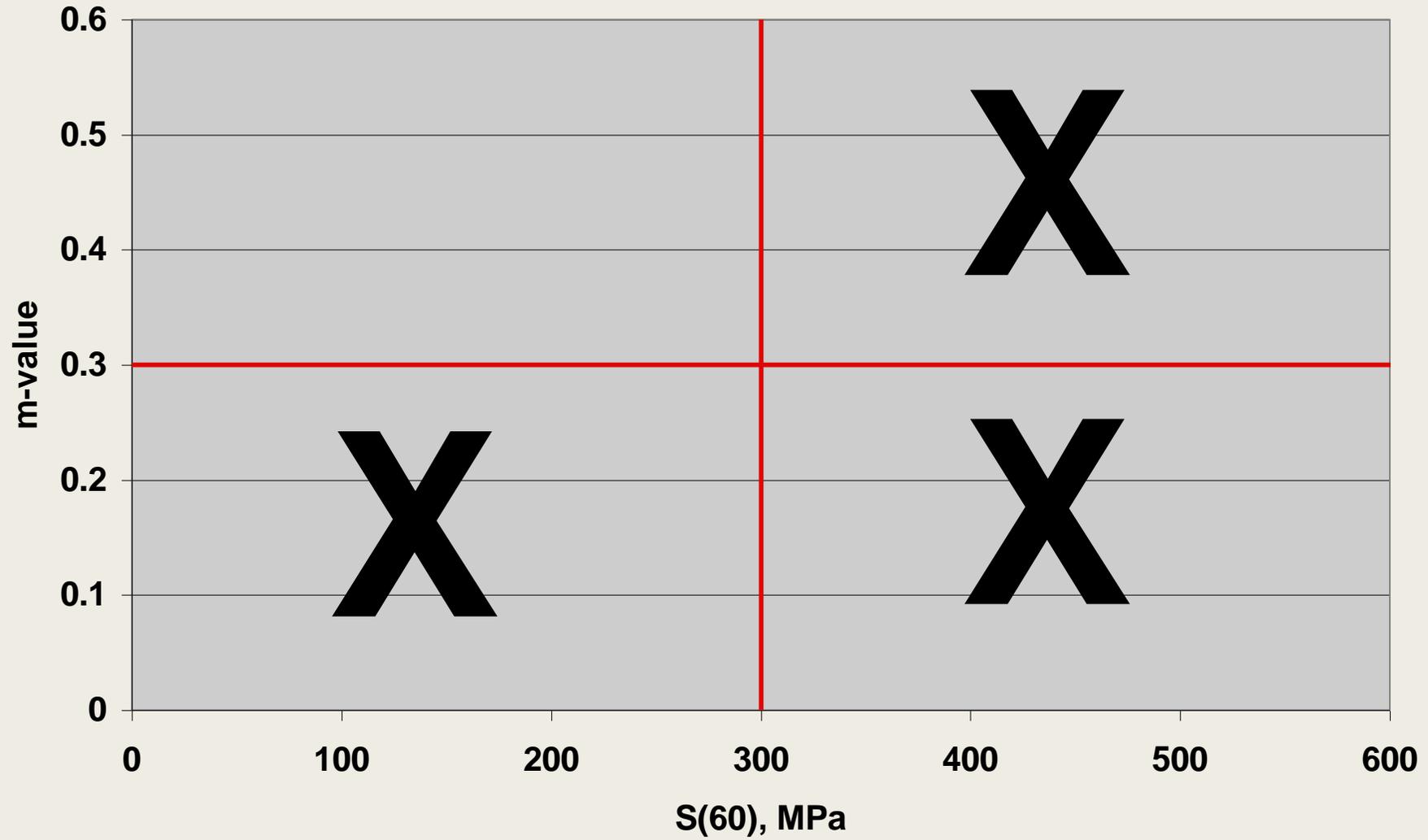


L x3.0k 30 um

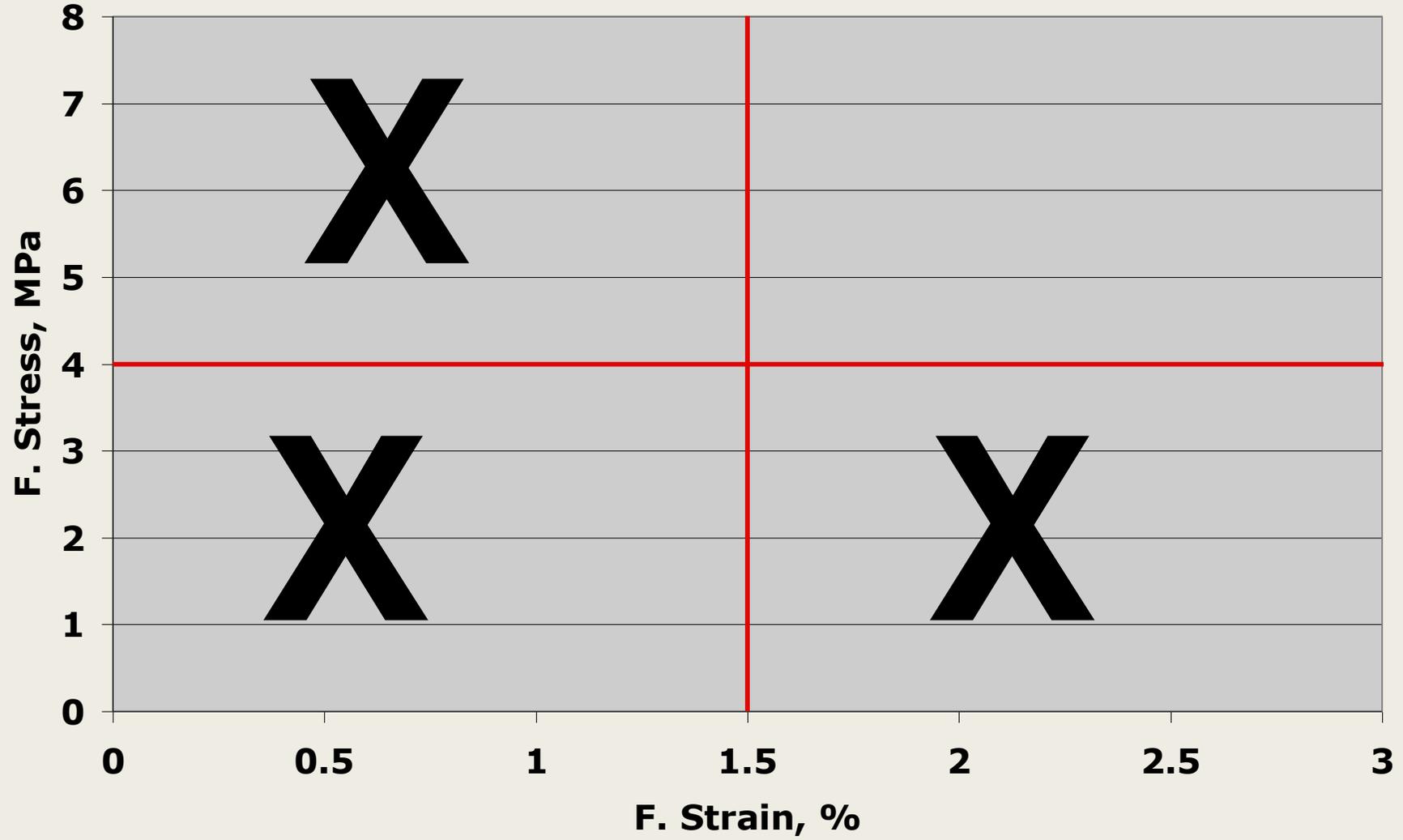
REOB – Recycled Engine Oil Bottoms

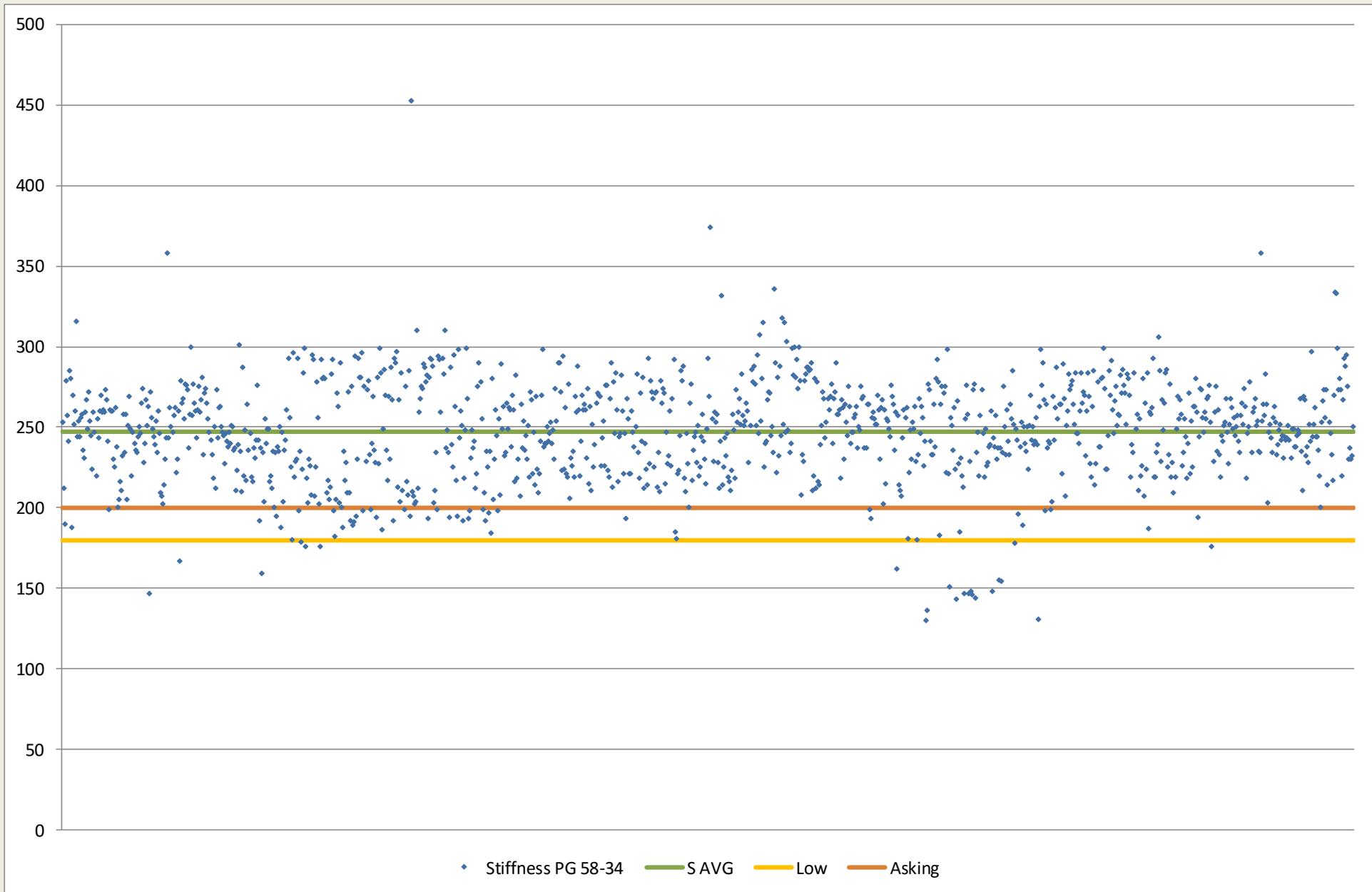
- What is the Issue? (pre Crude Oil price drop)
 - *I don't know!!*
 - I have not seen any field data showing effect of REOB on performance
 - The PG grading system forces use of soft base binders
 - There is a perception out there that excessive use of REOB is bad
- How is the Issue being addressed?
 - *Mix testing to show that either REOB is good or bad to performance*
 - The problem is most mix tests are strain controlled!!
 - So softer binders always look good!
- S and m-value based approach
 - *Specify that m-value is met at a certain S value*
- Double PAV – Embrittlement!

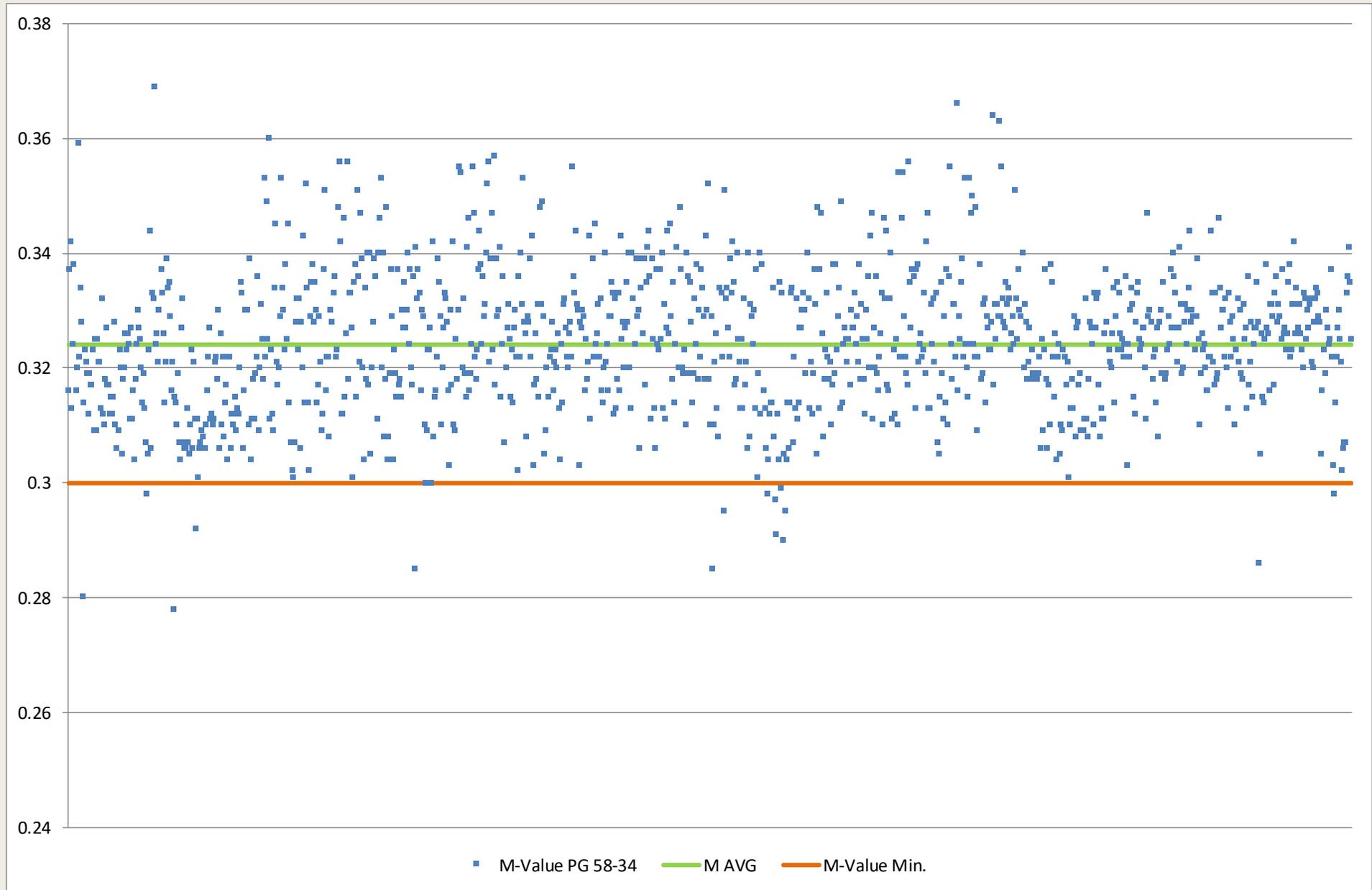
Low Temperature Specification M320 - Table 1

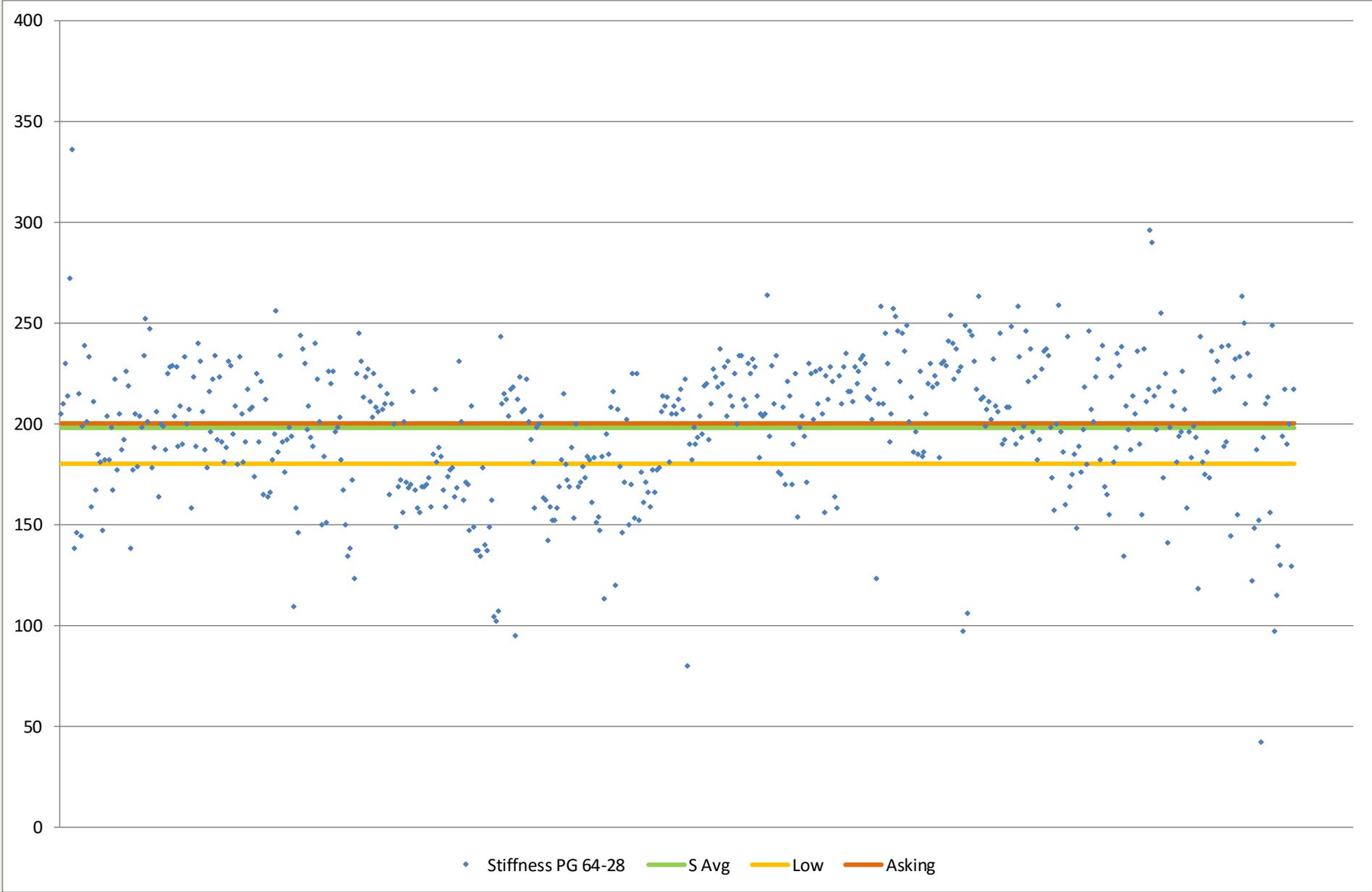


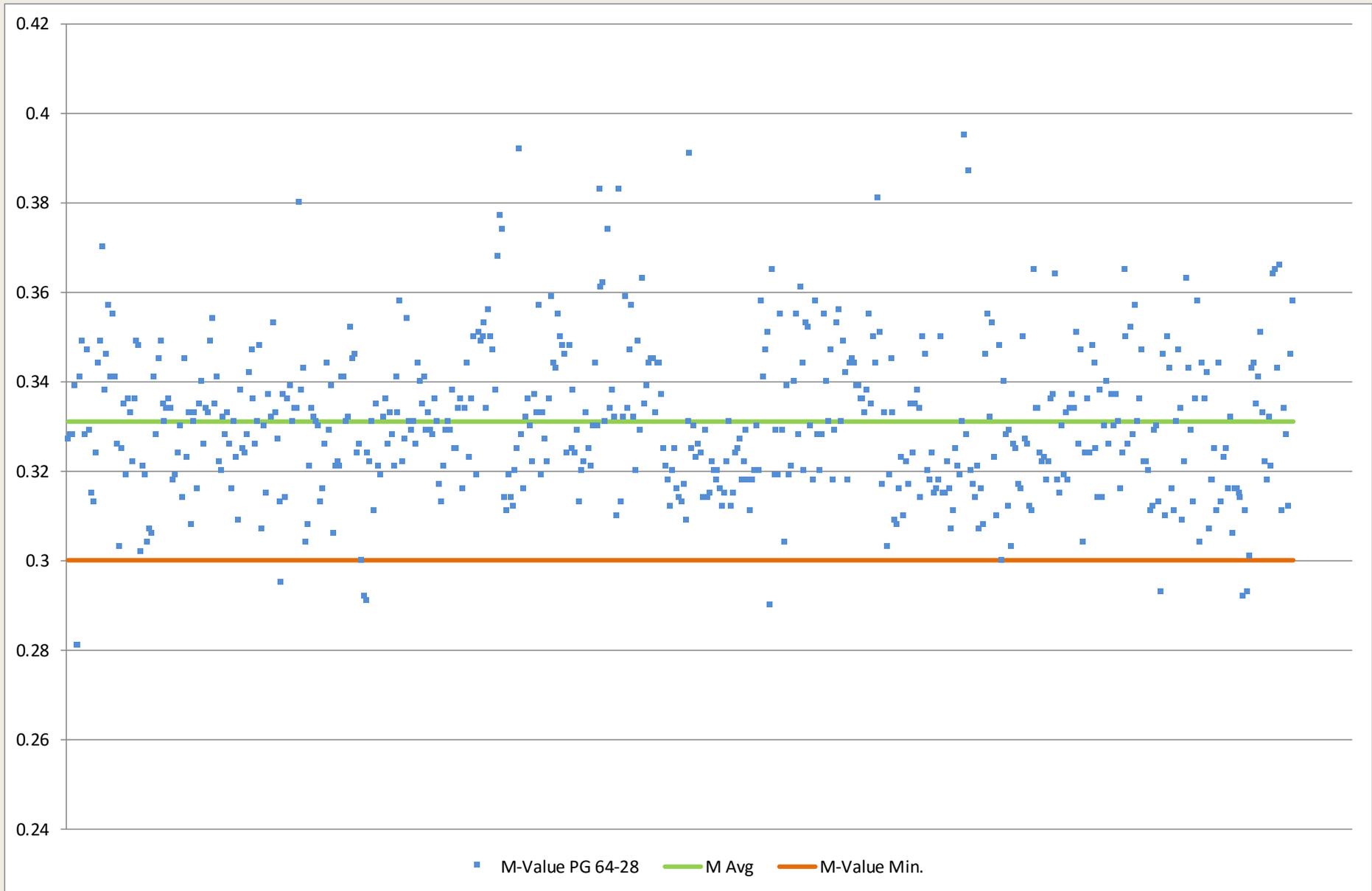
UDOT DTT Specification

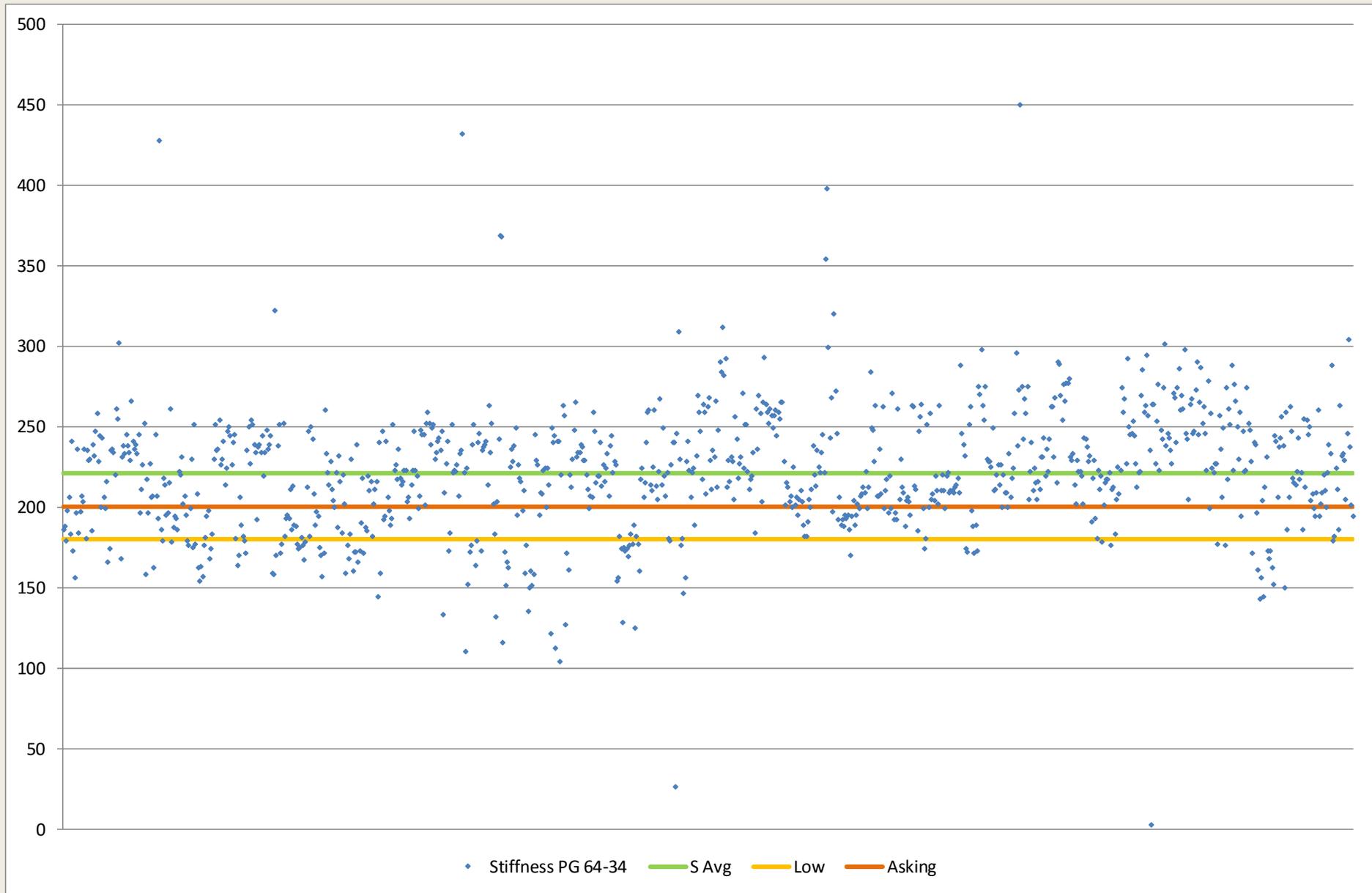


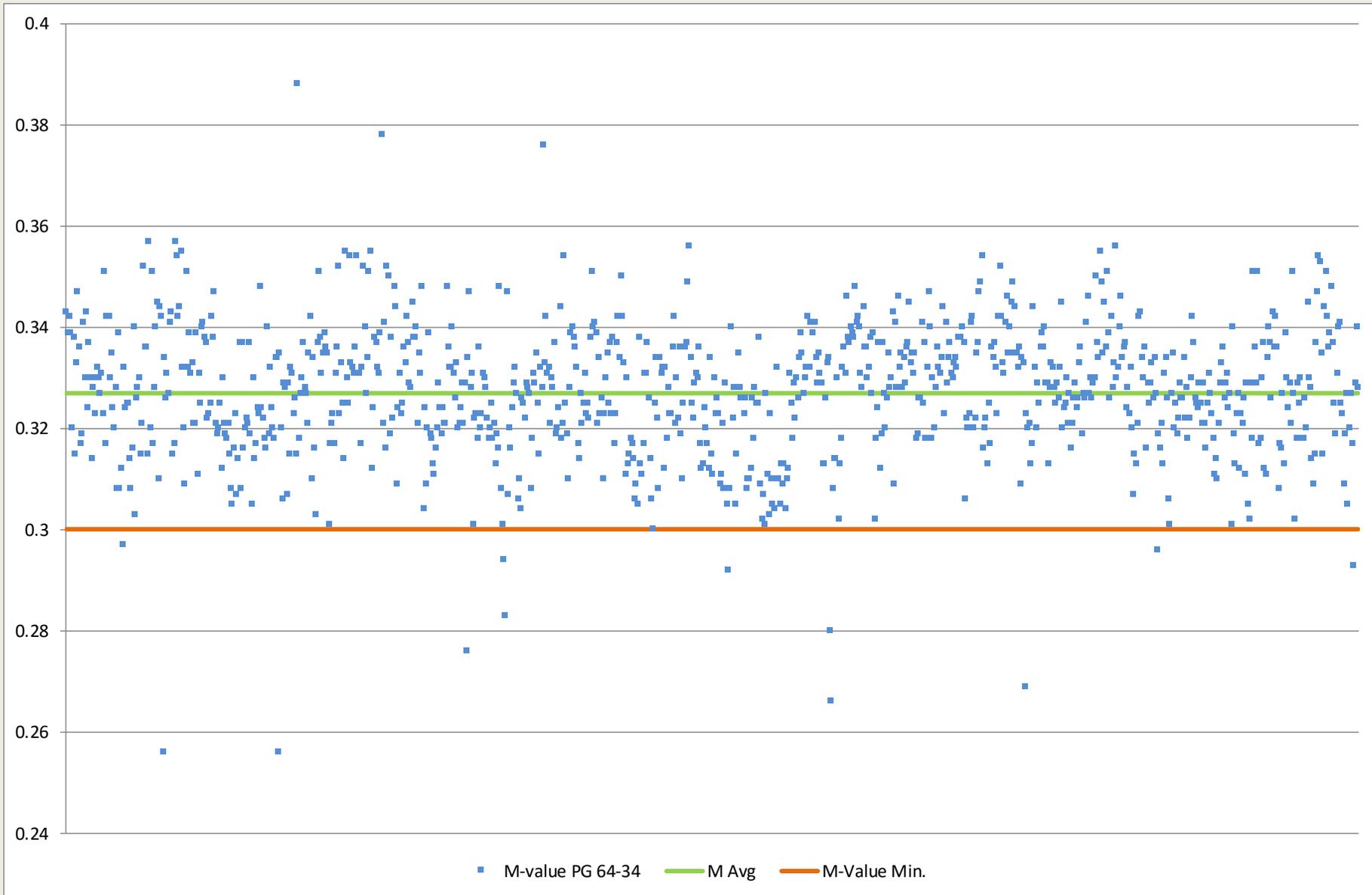


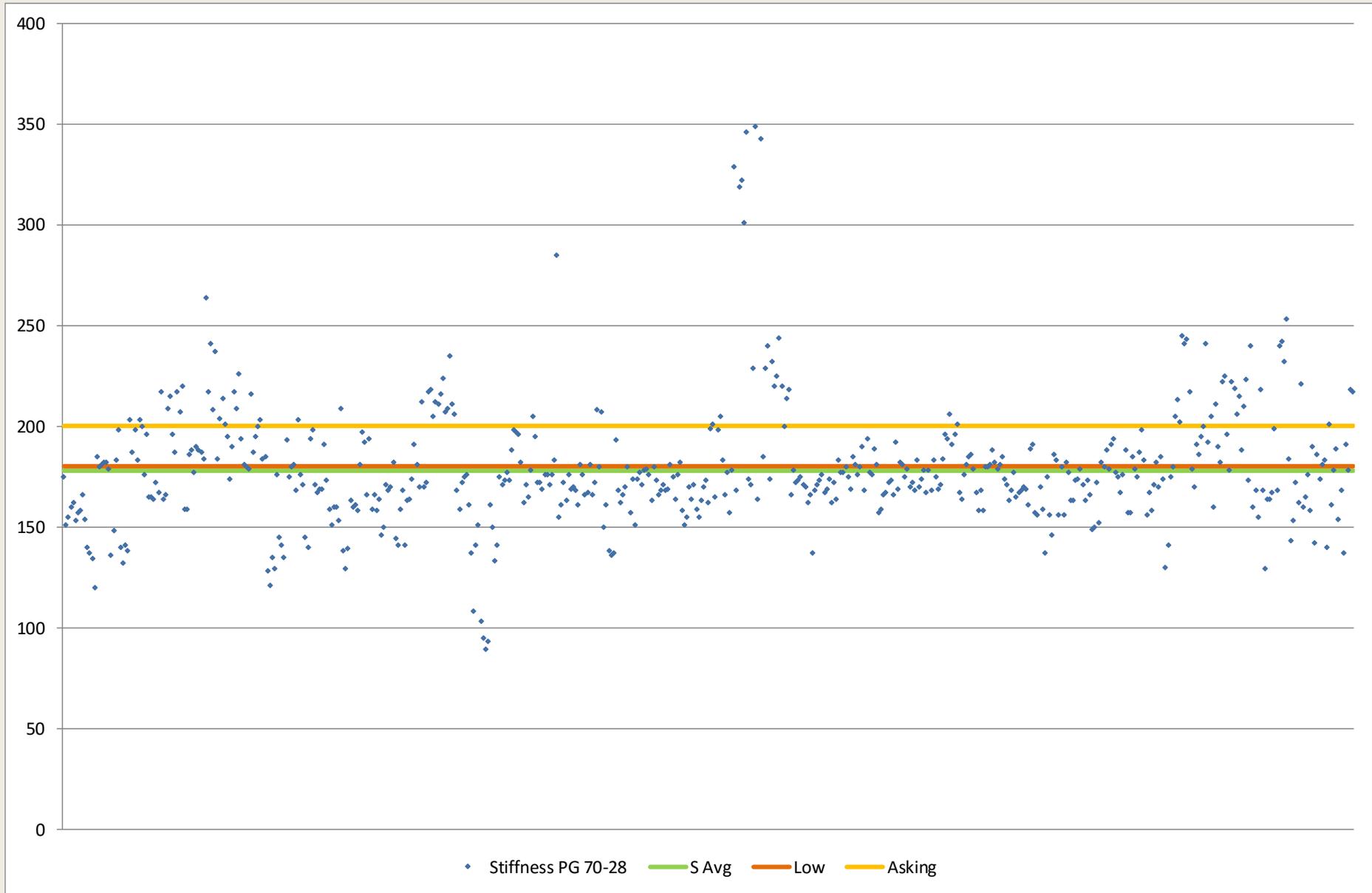


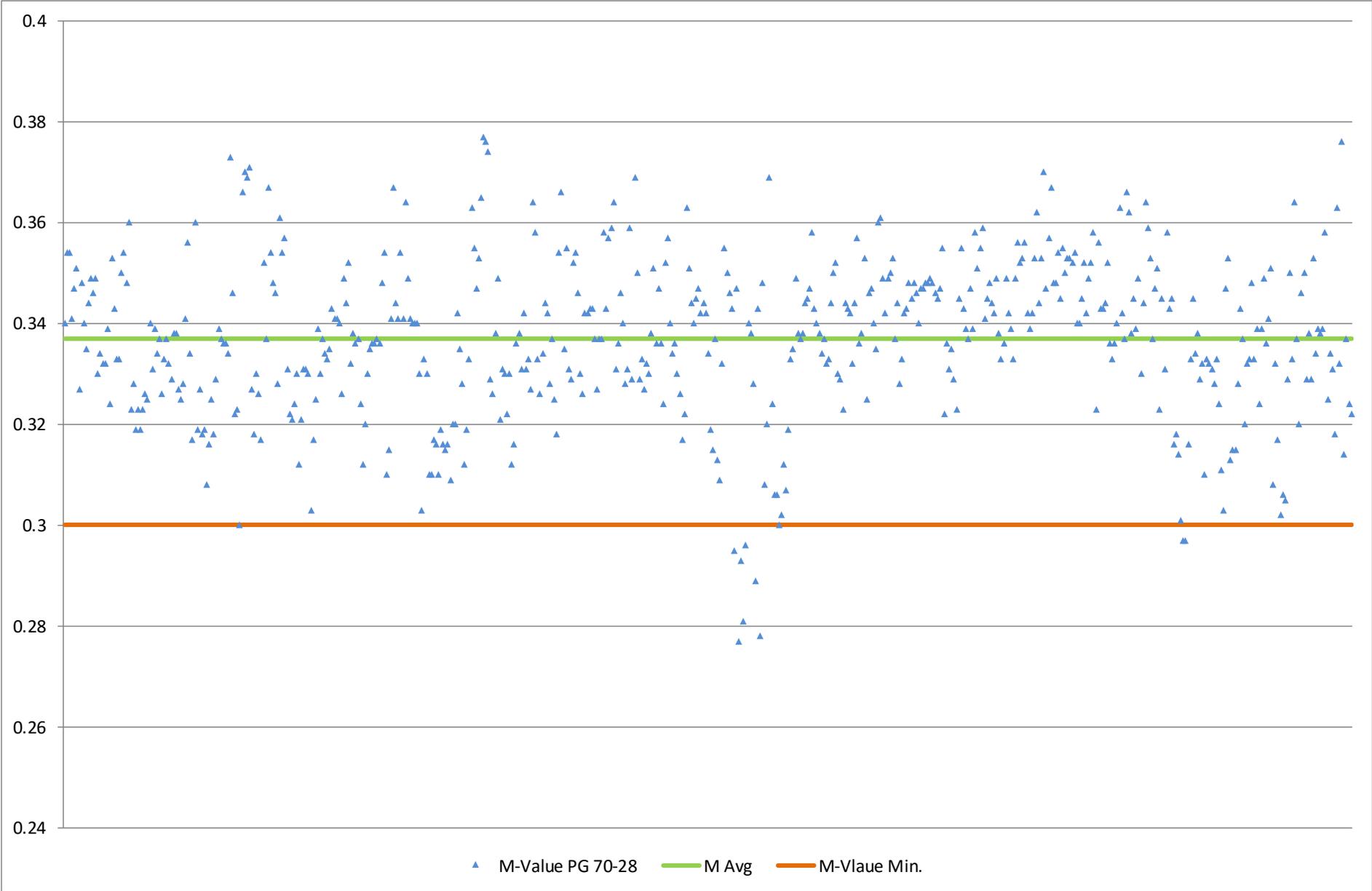






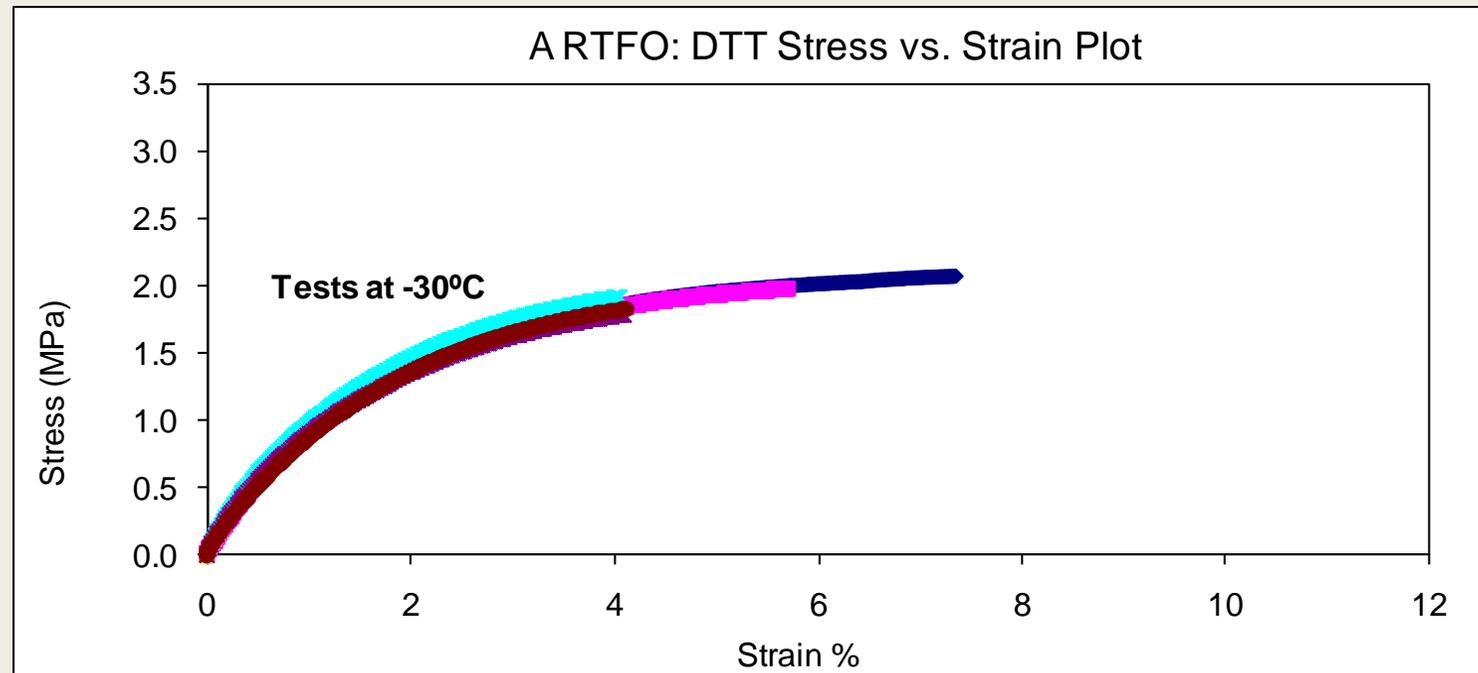
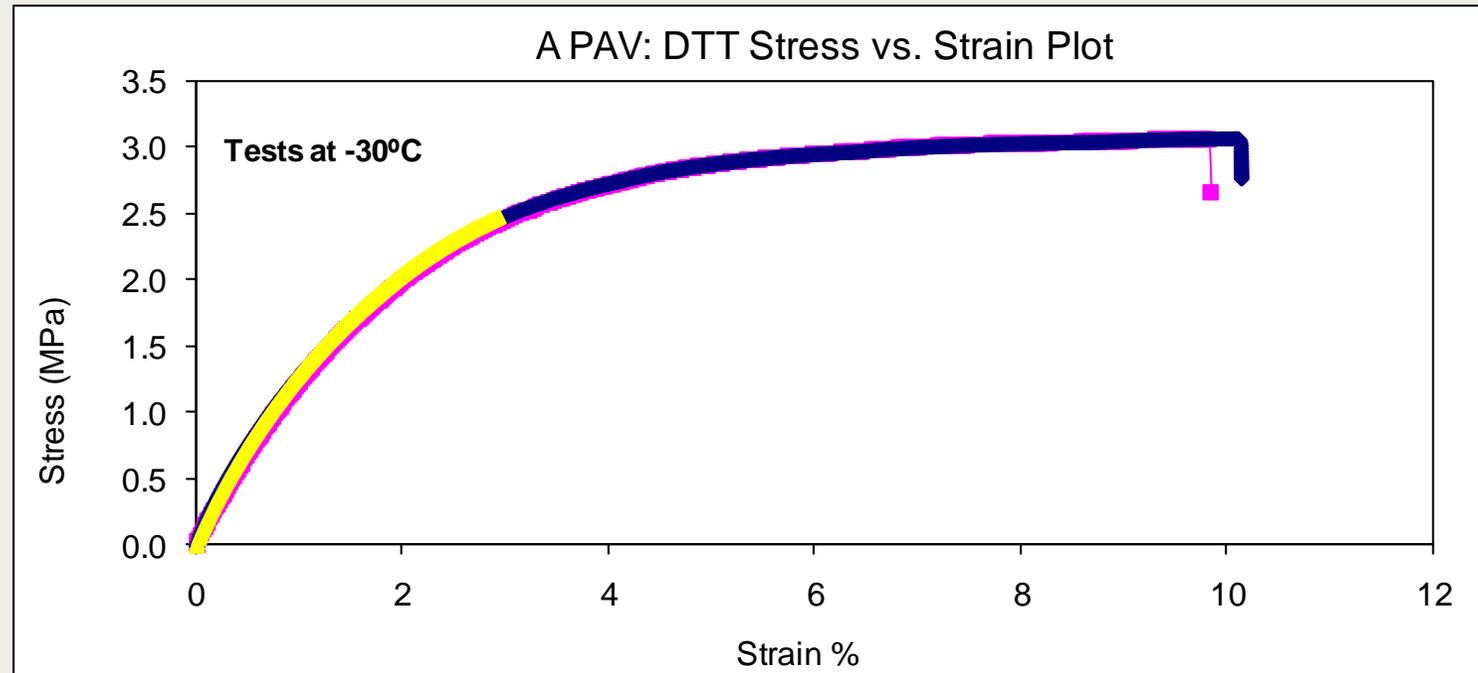




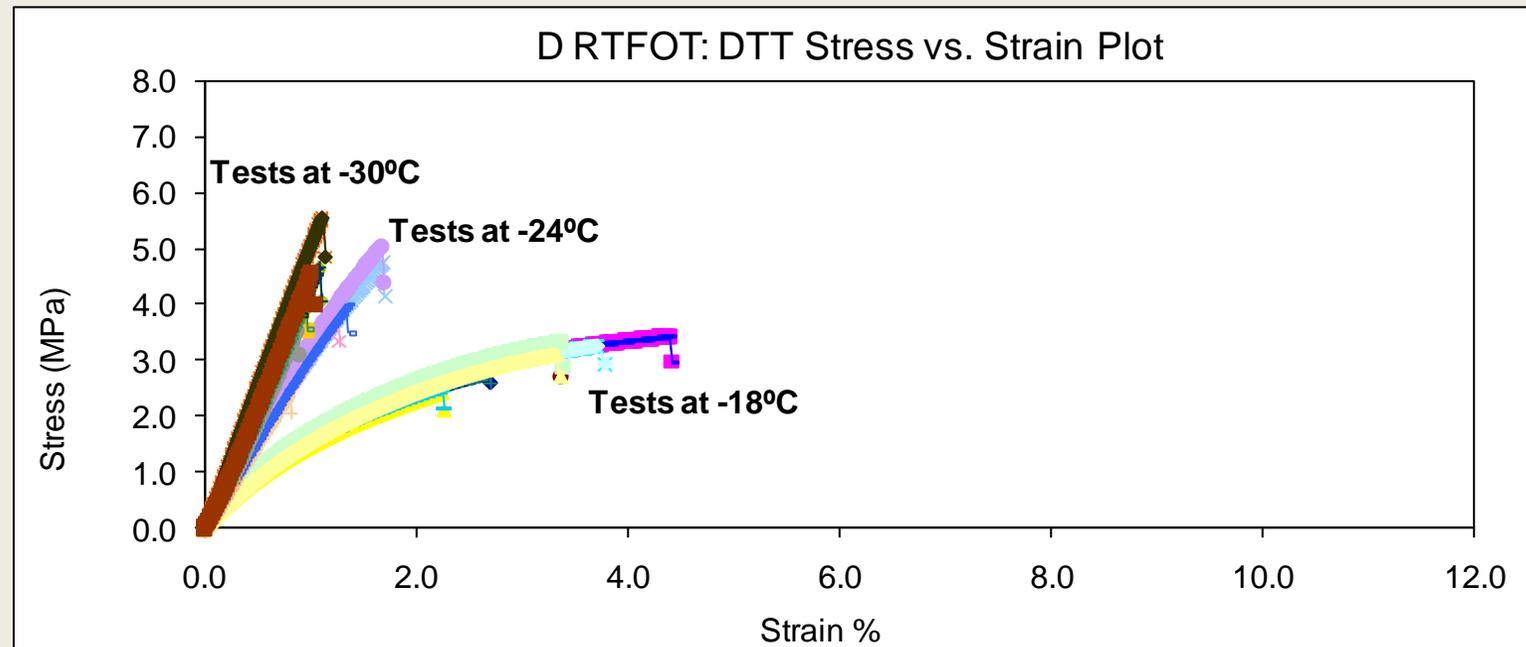
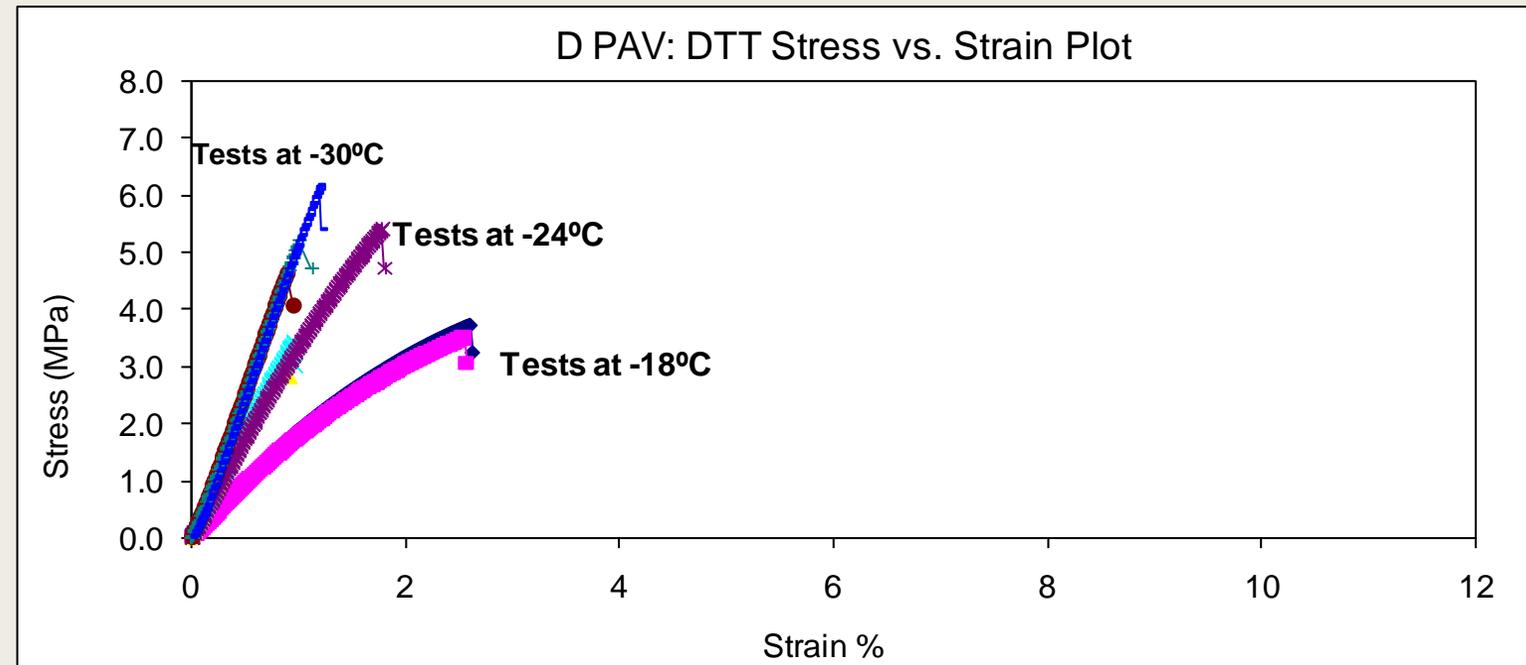


Binder Aging

- RTFOT Issues
 - *Binder spillout*
 - *NCHRP project to suggest alternatives*
 - SAFT, German Rolling Flask
- PAV Aging Issue -- Not enough aging!
 - *Does PAV really simulate Field Aging?*
 - DTT data says otherwise
- Double PAV
 - *REOB Issue driven*
- Bottom Line – Need to determine binder embrittlement due to aging as per field
 - *Glover Rowe Parameter*



PG 58-28 plain #1



Binder Fatigue – 20 years and Counting!

- Latest NCHRP Project to study binder aging
 - *AAT and NCAT*
 - *Tasked with developing a binder fatigue specification/test*
- DENT Test
 - *Notched ductility*
 - *Shown to relate to field performance*
- LAS Test
 - *DSR based strain sweep test*
 - *Has problems with adhesion of sample to plates!*
- Bottom Line – Need to look at binder embrittlement or fracture toughness

My Take – Binder Specification Issues

- MSCR

- *Needs to be implemented at all agencies*
- *Grade bumping is eliminated*
- *Polymer use is optimized*
 - Sensitive to formulation
 - Encourages well formulated PMAs

- REOB

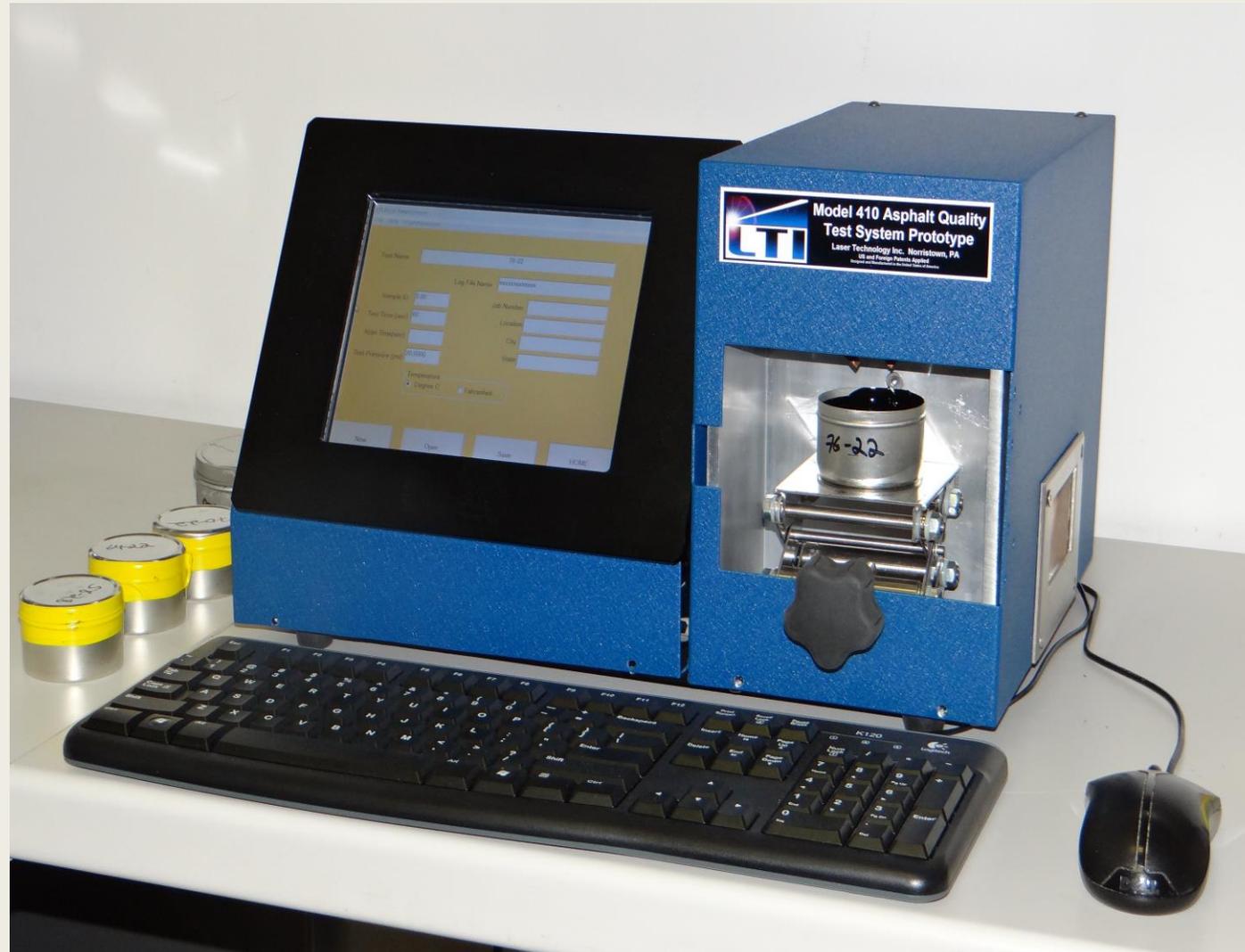
- *Need to analyze existing S and m-value data from all State Agencies*
 - Jack and I are looking into this.
 - If needed we can consider putting a range on S value where m-value is 0.3

My Take – Binder Specification Issues

- Binder Aging
 - *PAV needs tweaking*
 - *Nobody knows for sure what PAV aging really represents (5 yrs, 8 yrs, etc)*
 - *A soft asphalt remains a soft asphalt after RTFO and PAV aging!!*
 - There is no criss-crossing!
- Binder Fatigue
 - *Fatigue is best handled as a mix issue*
 - AC content sensitivity
 - Air voids, VMA and other mix additives also affect fatigue!
- Bottom Line – We need to look into QC tests for binders and mixes

New QC Tests for Binders and Mix

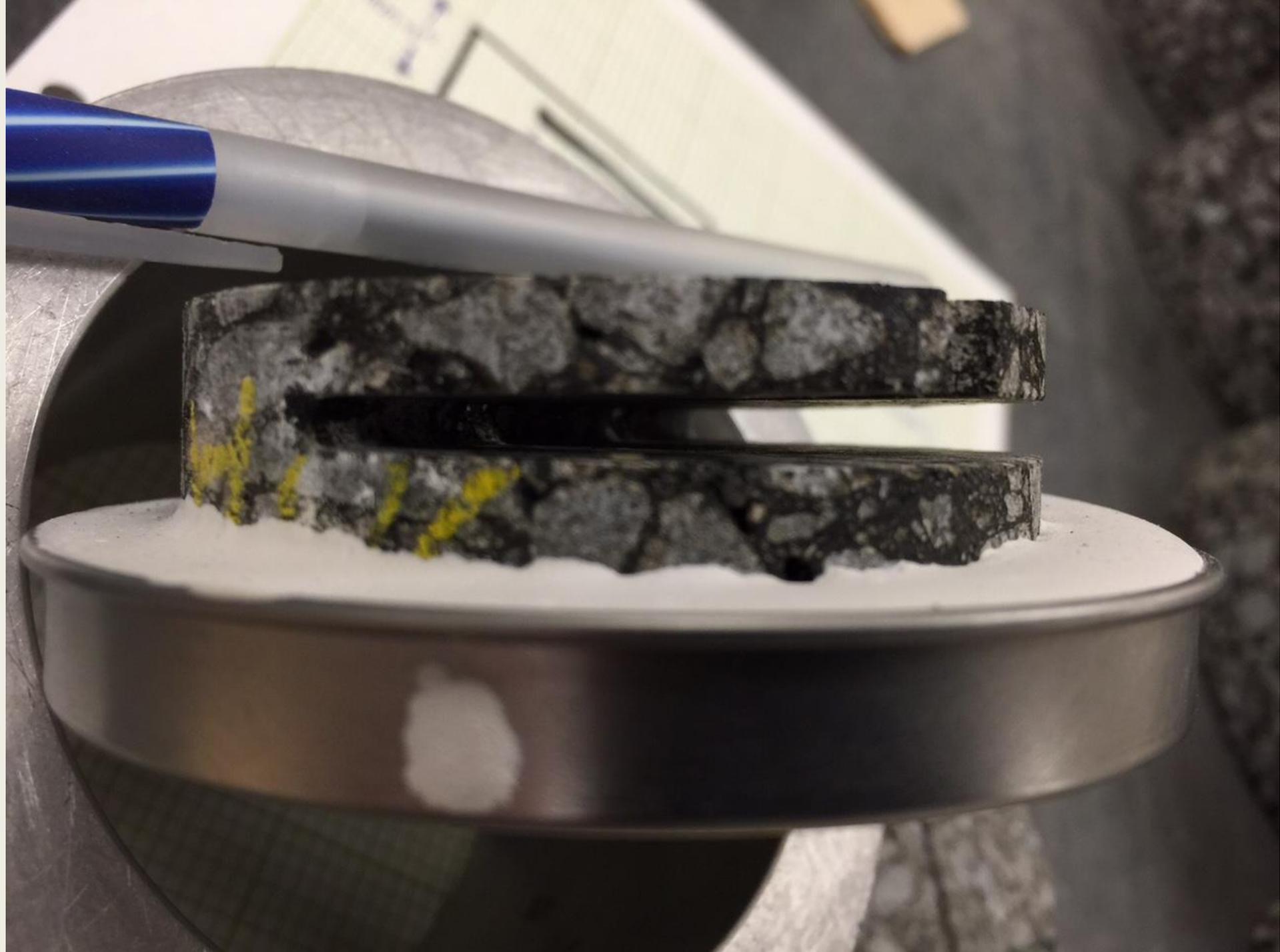
- Dongre Workability Test 'DWT' for mixes
 - *Based on existing Gyratory compactor*
 - *Determines Mix Workability*
 - *Also sensitive to AV, VMA, AC content, Mix Design*
- Binder and Mix QC Test
 - *Easy to use and portable*
 - *Innovative concept based on Air pressure and Laser*
 - *Produces Creep and Recovery data*



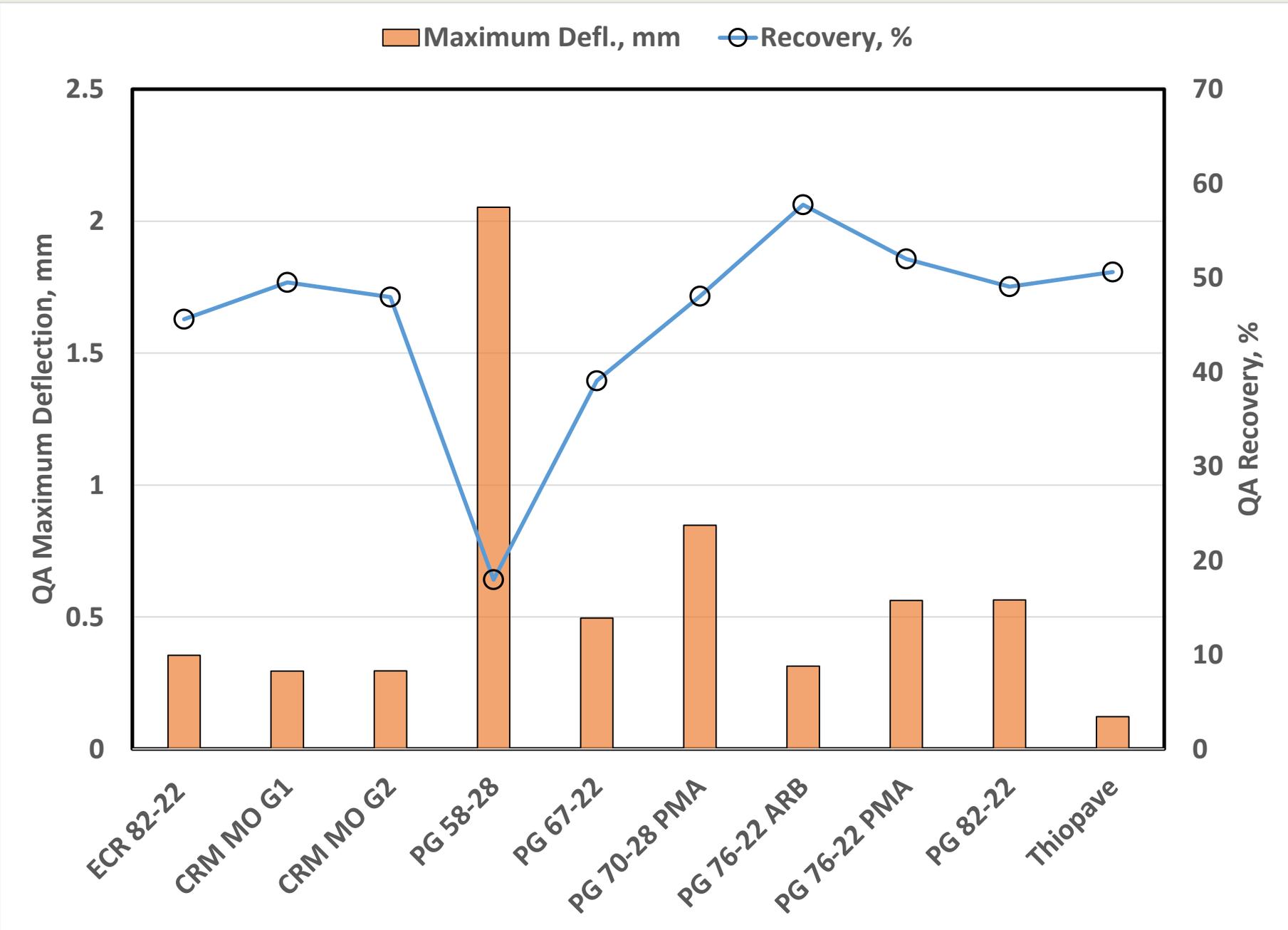
Binder Quality Control Tester

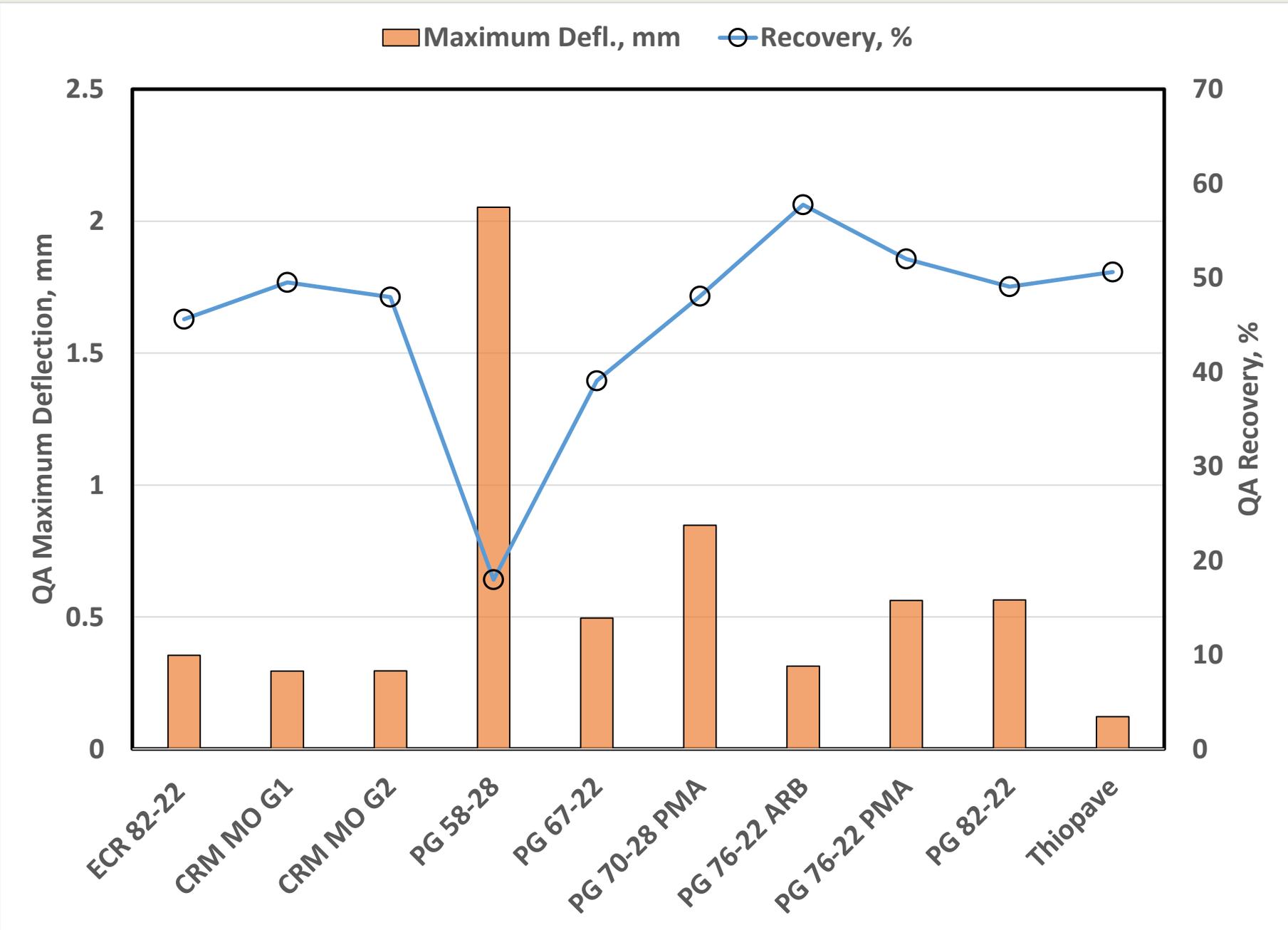
repeatability of qc data

Binder ID	Binder Type	Number of Replicates	QCT Max. Deflection, mm			QCT % Recovery		
			Average	Std. Dev	COV %	Average	Std. Dev	COV %
200/300 Pen	UnModified	5	2.8598	0.0437	2	14.4	0.4	3
#1 PG 58-28		5	0.5929	0.0370	6	20.1	1.0	5
PG 64-22		5	0.1588	0.0032	2	41.5	0.9	2
PG 76-10		5	0.0092	0.0006	6	82.0	7.8	10
#2 PG 58-28		5	0.7638	0.0192	3	15.5	0.1	1
PG 64-34	PMA	4	0.3383	0.0058	2	77.4	0.7	1
PG 76-22		5	0.0689	0.0023	3	58.0	1.1	2
PG 82-22	Crumb Rubber Modified	5	0.0533	0.0030	6	57.3	2.5	4
#1 PG 76-22		2	0.1377	0.0049	4	54.7	1.2	2
#2 PG 76-22		2	0.1055	0.0028	3	57.3	1.1	2
#3 PG 76-22		2	0.0908	0.0009	1	59.9	1.8	3
Pooled Average					3			3











THANK YOU!

Questions?